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Topics

CATT-Acoustic DLL Directivity Interface (DDI)

DDI verification examples

Conclusions

Acknowledgements

CATT-Acoustic DLL Directivity Interface (DDI)

DLL = Dynamic Link Library = a.k.a. "Plug-in"

Background

- Many types of complex sound sources have extended near-fields (may extend up to > 100 m for some designs):
 - large arrays
 - V-DOSC
 - distributed mode loudspeakers

- A single *3D-balloon* at 10°, 5° or 1° resolution is not sufficient:
 - a 3D-balloon measured at e.g. 10 m distance can be <u>10-20 dB in</u> error in the main lobe at other distances
 - even a 1° resolution would not solve the problem since it lies in the fixed measurement distance
- Many array designs are based on DSP for beam-steering:
 - hundreds of possible beam shapes and angles to measure them all would be a very big task

Implementation

- The CATT-Acoustic Win32 DLL Directivity Interface (DDI) enables:
 - distance dependent directivity (i.e. handling of the near-field)
 - any angular resolution
 - any frequency resolution (from high-res FIRs to 1/1-octaves)
 - hiding of intellectual property (e.g. beam-steering methods)
 - generic array modeling based on individual element 3D position and aim, directivity in 15° polars or 10° full-space formats, octave-band or FIR-filter weight, delay
 - **specific array modeling** based on detailed manufacturer specifications allowing for beam-steering of e.g. **azimuth**, **focusdistance**, **openingangle**

- **interpolated models** based on a set of 10° 3D-ballons. A less accurate but much faster way of modeling arrays
- **analytically modeled sources** (line sources, multi-pole expansions, spherical harmonics, synthesized instruments etc.)
- optional **3D description** of sources (not yet implemented but the interface can be added to using a version-checking API)
- dedicated brand/model help
- intended to be an **open interface**

• Current utilization of the DDI in *CATT-Acoustic v7.2*:

- the result of the coherent run-time array summation is used for direct sound and first order reflections
- the far-field directivity is used for higher order reflections

However:

- <u>only if a reflection takes place on a big, hard and smooth</u> <u>surface</u> the coherent summation of all array elements is valid
- reflections in small surfaces (where only part of the array actually is reflected) or in rough surfaces (that scatters the reflection)
 destroy the relationship between the sources in the array and the free-field directivity is no longer valid
- how to best handle late reflections with array modeling is <u>a problem</u>
 <u>little discussed</u> and not yet solved



Array

Octave-band averaged 1kHz directivity



CATT-Acoustic DLL Directivity Interface (DDI)

108th AES Convention, Paris February 2000

Octave-band averaged 1kHz directivity



Comparison between Run-time DDI, Interpolated DDI and 10° far-field balloon





Same scale: comparing level



Detailed scale: comparing pattern

Verification examples

- Free field SPL on-axis as a function of distance
- Two kinds of PA-system verifications:
 - four 2.7 m long 16-element *Duran Audio Intellivox 2c* DSP-controlled column arrays in a 160 m long trainstation (Lille, France)
 - two Intellivox 2c and two Intellivox 4c (4.35 m long) DSP-controlled column arrays in a 1^{3th} century church with 6 sec reverberation time (Skara, Sweden).

Octave-band averaged 1kHz on-axis free field SPL

Duran Audio Intellivox 2c 2.7 m long DSP-controlled column array DSP settings: azimuth = 0°, focusdistance = 40 m, openingangle = 8° Outdoor measurements by Duran Audio



 An installation of four *Intellivox 2c* (DSP-controlled 16-element column arrays) in the Lille Flandres railway station. RASTI measured for 49 locations using *MLSSA*:







 in the railway station the overall RASTI level is slightly overestimated as can be attributed to a number of uncertainties and simplifications of the room model as well as to the problem of handling array modeling for higher order reflections Installation of two Intellivox 2c (2.7 m long) and two Intellivox 4c (4.35 m long) columns in a 13th century church with 6 sec reverberation time (Skara, Sweden). <u>Much simplified room model (see photo)</u>



 RASTI values show good agreement and DDI run-time modeling is consistently better than fixed 10° fullspace. However, farreaching conclusions cannot be drawn from a much simplified model of a complex church and with only 5 locations measured



Conclusions

- that the distance-dependent array-modeling matches the RASTI trend much better than fixed 10° far-field 3D-balloons
- that the good results from the interpolated DDI model indicates that the key for RASTI estimates using column arrays is not necessarily to have a high angular resolution but to handle the extended near-field. This conclusion is likely to be mostly valid for arrays of the type used here with small transducers and simple transducer directivities.
- For clustering of larger cabinets, with a more complex element directivity, a 10° or 5° element directivity without phase will be insufficient. For such arrays/clusters, also the array-modeling itself is much more complex (due to screening and diffraction effects etc.) but the DDI can handle it if the theory is known and if high-res data is available.

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